## Jet Propulsion Laboratory

Interoffice Memorandum
MISR SCIENCE DFM \#230
August 23, 2000
To: Carol Bruegge
From: Nadine C. Lu Chrien
Subject: On-Board Calibrator response functions used in Ancillary Radiometric Product In-flight Calibration version 4

CC: B. Chafin
The purpose of this memorandum is to document the response functions of the MISR on-board calibrator (OBC) utilized in computing the camera gain coefficients for ARP Version 4. The response functions are the diode étendue or $\mathrm{A} \Omega$, the diode integrated solar-weighted spectral response, and the diode calibration correction factors. Also, included are the factors required to convert from ARP Version 3 radiances to ARP Version 4 radiances.

The diode integrated solar-weighted spectral response (Table 1) is defined in equation 1 . Where $E_{0, \lambda}$ is the exo-atmospheric solar irradiance and $R_{\lambda}$ is the diode spectral response.

$$
\begin{equation*}
\mathfrak{R}=\int_{200 \mathrm{~nm}}^{1200 \mathrm{~nm}} E_{0, \lambda} R_{\lambda} \lambda d \lambda \tag{1}
\end{equation*}
$$

The diode étendue or $\mathrm{A} \Omega$ is the area-projected solid angle product for the photodiode (Table 2).The diode calibration correction factors (Table 3) are multiplicative factors that are applied to the product of the diode $\mathrm{A} \Omega$ and the diode integrated solar-weighted spectral response. The preflight calibration of the blue HQE diode is used as the standard to which the other photodiodes are calibrated. The Ddiodes are calibrated using the goniometer to provide a transfer calibration. The OBC data collected during orbits 1259 and 1912 for Cal-North and Cal-South respectively were used. The calibration correction factors represent the average correction factor computed for Cal-North and Cal-South with the exception of the D-diode factors. For the D-diode factors, the north-south average is applied to the PIN-G for the transfer, but PIN-3 only views the south panel and PIN-4 only views the north panel.
The radiance measured by a given photodiode is computed following equation 2 where $k$ is the calibration correction factor. The calibration correction factor is computed based upon the assumption that the Spectralon® calibration panels are spectrally flat, Lambertian targets. This implies that the ratio of one diode current to another should equal the ratio of étendue-response products, $\mathrm{A} \Omega \Re$ (equation 3). The calibration correction factors for the nadir viewing diodes are computed using the blue HQE diode and its preflight calibration as the standard, i.e., $k_{\mathrm{HQE}, \text { blue }}=1$ (equation 4). The D-diodes, PIN-3 and PIN-4, are calibrated to the blue HQE diode using the goniometer, PIN-G, as a transfer standard. The goniometer calibration correction factor is computed using currents when the goniometer position is nadir-viewing. The D -diode bands are then calibrated to the goniometer diode bands as shown in equation 5 .

$$
\begin{equation*}
L^{\mathrm{std}, \mathrm{OBC}}=\frac{1.2395 i E_{0}^{\text {std }}}{(A \Omega \Re) \cdot k} \tag{2}
\end{equation*}
$$

$$
\begin{gather*}
{\left[\frac{i_{2}}{(A \Omega \Re)_{2} \cdot k_{2}}=\frac{L_{2}^{\text {std,OBC }}}{E_{0,2}^{\text {std }}}=\frac{L_{1}^{\text {std,OBC }}}{E_{0,1}^{\text {std }}}=\frac{i_{1}}{(A \Omega \Re)_{1} \cdot k_{1}}\right] \Rightarrow\left(\frac{i_{2}}{i_{1}}=\frac{(A \Omega \Re)_{2}}{(A \Omega \Re)_{1}} \cdot \frac{k_{2}}{k_{1}}\right)}  \tag{3}\\
k_{\text {diode, band }}=\frac{i_{\text {diode, band }}^{i_{\mathrm{HQE}, \text { blue }}} \div \frac{(A \Omega \Re)_{\text {diode, band }}}{(A \Omega \Re)_{\mathrm{HQE}, \text { blue }}}}{k_{\mathrm{D}-\text { diode,band }}=\frac{i_{\text {D-diode,band }}}{i_{\text {goni, band @D-angle }}} \div \frac{(A \Omega \Re)_{\mathrm{D}-\text { diode,band }}}{(A \Omega \Re)_{\text {goni, band }} \cdot k_{\text {goni, band }}}} \tag{4}
\end{gather*}
$$

Table 1: diode integrated solar-weighted spectral response, $\mathfrak{R}\left[\mathrm{W} \mathrm{m}^{-1}\right]$

| diode |  | Band |  |  |  |  |  |  |  |
| ---: | ---: | ---: | ---: | ---: | ---: | :---: | :---: | :---: | :---: |
| position | type | BLUE |  |  |  |  | GREEN | RED | NIR |
| +Y | PIN-1 | 13.0698 | 14.3526 | 8.7570 | 11.4217 |  |  |  |  |
| -Y | PIN-2 | 13.0104 | 14.9508 | 8.7721 | 12.1682 |  |  |  |  |
| Df | PIN-3 | 15.4890 | 14.5350 | 8.6580 | 11.5130 |  |  |  |  |
| Da | PIN-4 | 16.0568 | 15.5577 | 10.8097 | 11.6961 |  |  |  |  |
| goniometer | PIN-G | 12.6824 | 14.2086 | 11.1406 | 10.9881 |  |  |  |  |
| $+\mathrm{Y}(\mathrm{B}, \mathrm{G})$, <br> $-\mathrm{Y}(\mathrm{R}, \mathrm{N})$ | HQE | 17.3235 | 11.6565 | 12.5182 | 16.1813 |  |  |  |  |

Table 2: diode étendue or $\mathrm{A} \Omega$ [ $\left.\mathrm{m}^{2} \mathrm{sr}\right]$

| Diode |  | Band |  |  |  |
| ---: | ---: | ---: | :---: | :---: | :---: |
| position | type | BLUE | GREEN | RED | NIR |
| +Y | PIN-1 | $1.4806 \mathrm{E}-08$ | $1.4829 \mathrm{E}-08$ | $1.4755 \mathrm{E}-08$ | $1.4653 \mathrm{E}-08$ |
| -Y | PIN-2 | $1.4803 \mathrm{E}-08$ | $1.4813 \mathrm{E}-08$ | $1.4766 \mathrm{E}-08$ | $1.4674 \mathrm{E}-08$ |
| Df | PIN-3 | $1.4786 \mathrm{E}-08$ | $1.4793 \mathrm{E}-08$ | $1.4738 \mathrm{E}-08$ | $1.4623 \mathrm{E}-08$ |
| Da | PIN-4 | $1.4752 \mathrm{E}-08$ | $1.4783 \mathrm{E}-08$ | $1.4786 \mathrm{E}-08$ | $1.4783 \mathrm{E}-08$ |
| goniometer | PIN-G | $1.4796 \mathrm{E}-08$ | $1.4830 \mathrm{E}-08$ | $1.4806 \mathrm{E}-08$ | $1.4779 \mathrm{E}-08$ |
| +Y (B, G $),$ <br> $-\mathrm{Y}(\mathrm{R}, \mathrm{N})$ | HQE | $7.4541 \mathrm{E}-09$ | $7.4495 \mathrm{E}-09$ | $7.4719 \mathrm{E}-09$ | $7.4730 \mathrm{E}-09$ |

Table 3: diode calibration correction factors
computed using Orbits 1259 (Cal-North) and 1912 (Cal-South), HQE blue as standard

| Diode |  | Band |  |  |  |
| ---: | ---: | ---: | ---: | ---: | ---: |
| position | type | BLUE | GREEN | RED | NIR |
| +Y | PIN-1 | 0.8930 | 0.8871 | 0.9179 | 0.8943 |
| -Y | PIN-2 | 0.8993 | 0.8472 | 0.8999 | 0.8543 |
| Df | PIN-3 | 0.8637 | 0.8645 | 0.9119 | 0.8937 |
| Da | PIN-4 | 0.8375 | 0.8268 | 0.8937 | 0.8660 |
| goniometer | PIN-G | 0.9030 | 0.8905 | 0.8953 | 0.8854 |
| $+Y(B, G)$, <br> $-Y(R, N)$ | HQE | 1.0000 | 1.0337 | 0.9570 | 1.0792 |

To convert Version 3 radiances whose gain coefficients are based on the preflight diode response functions to Version 4 radiances which are based upon the diode response functions given here, one would multiply the Version 3 radiance by the appropriate factor from Table 4. The $\mathrm{G}_{1}$ coefficient channel means are given in Tables 5 and 6 for each of the two versions. Table 7 shows the percent difference between them.

$$
\begin{equation*}
L_{v 4}=L_{v 3} \cdot \frac{G_{1, v 3}}{G_{1, v 4}} \tag{6}
\end{equation*}
$$

Table 4: factors to convert from ARP version 3 radiances to version 4 radiances, $\frac{G_{1, v 3}}{G_{1, v 4}}$

| Camera | Band |  |  |  |
| :---: | ---: | ---: | ---: | ---: |
|  | Blue |  |  |  |
| Dreen | Red | NIR |  |  |
| Df | 0.9440 | 0.9579 | 0.9649 | 0.9347 |
| Cf | 1.0010 | 1.0164 | 0.9445 | 0.9287 |
| Bf | 1.0204 | 1.0401 | 1.0223 | 0.9872 |
| Af | 0.9987 | 0.9962 | 1.0001 | 0.9574 |
| An | 0.9284 | 0.9553 | 0.9812 | 0.9624 |
| Aa | 1.0309 | 1.0069 | 1.0495 | 0.9860 |
| Ba | 1.0501 | 0.9797 | 1.0392 | 0.9698 |
| Ca | 0.9905 | 1.0553 | 1.0309 | 0.9844 |
| Da | 1.0159 | 1.0714 | 1.0699 | 1.0057 |

Table 5: G1 coefficient, channel mean: MISR_AM1_ARP_INFLTCAL_F01_001.hdf ( $G_{1, v 3}$ )

| Camera | Band |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Blue | Green | Red | NIR |
| Df | 23.7327 | 23.5022 | 28.0790 | 44.1225 |
| Cf | 23.2061 | 24.0454 | 29.5118 | 44.9768 |
| Bf | 23.6779 | 22.6386 | 29.4522 | 45.6965 |
| Af | 23.4319 | 23.6168 | 29.2569 | 43.8165 |
| An | 20.9298 | 21.9385 | 30.2010 | 43.7020 |
| Aa | 23.1797 | 24.3174 | 28.9184 | 42.7098 |
| Ba | 26.0574 | 23.7955 | 27.5437 | 47.8591 |
| Ca | 23.0300 | 23.0991 | 27.9198 | 44.6848 |
| Da | 23.0859 | 22.7480 | 27.4547 | 42.3987 |

Table 6: G1 coefficient, channel mean: MISR_AM1_ARP_INFLTCAL_T002_F01_004c.hdf ( $G_{1, v 4}$ )

| Camera | Band |  |  |  |
| :---: | ---: | ---: | ---: | ---: |
|  | Blue |  |  |  |
| Dreen | Red |  |  |  |
| Df | 25.1400 | 24.5340 | 29.1016 | 47.2038 |
| Cf | 23.1820 | 23.6575 | 31.2472 | 48.4285 |
| Bf | 23.2045 | 21.7657 | 28.8087 | 46.2912 |
| Af | 23.4616 | 23.7062 | 29.2541 | 45.7679 |
| An | 22.5434 | 22.9652 | 30.7784 | 45.4112 |
| Aa | 22.4853 | 24.1517 | 27.5552 | 43.3149 |
| Ba | 24.8146 | 24.2892 | 26.5047 | 49.3487 |
| Ca | 23.2513 | 21.8879 | 27.0821 | 45.3921 |
| Da | 22.7255 | 21.2316 | 25.6618 | 42.1603 |

Table 7: G1 coefficient, channel mean: Percent difference between v3 and v4, [\%]

| Camera | Band |  |  |  |  |  |  |
| :---: | ---: | ---: | ---: | ---: | :---: | :---: | :---: |
|  | Blue |  |  |  |  |  |  |
| Df | 5.9 | Green |  |  |  | Red | NIR |
| Cf | -0.1 | -1.6 | 3.6 | 7.0 |  |  |  |
| Bf | -2.0 | -3.9 | 5.9 | 7.7 |  |  |  |
| Af | 0.1 | 0.4 | -2.2 | 1.3 |  |  |  |
| An | 7.7 | 4.7 | 0.0 | 4.5 |  |  |  |
| Aa | -3.0 | -0.7 | -4.7 | 3.9 |  |  |  |
| Ba | -4.8 | 2.1 | -3.8 | 1.4 |  |  |  |
| Ca | 1.0 | -5.2 | -3.0 | 3.1 |  |  |  |
| Da | -1.6 | -6.7 | -6.5 | 1.6 |  |  |  |
|  |  |  | -0.6 |  |  |  |  |

